



Office: - 304, Vastu Pooja CHS, Near Raut Chawl, Barrage Road, Kulgaon, Badlapur (West) Dist. - Thane 421503 Maharashtra (India) Email ID: - <u>reliableeng7@gmail.com</u> <u>reliablegeotechnic@outlook.com</u> _Contact: +91-9987193247 +91-9172214249

GEOTECHNICAL INVESTIGATION REPORT

GEOTECHNICAL INVESTIGATION FOR

PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA

> CLIENT M/s. MASTERS AND ASSOCIATES

GEOTECHNICAL INVESTIGATION AND REPORT SUBMITTED BY M/s. RELIABLE ENGINEERING 304, VASTU POOJA BUILDING, NEAR RAUT CHAWL, BARRGAE ROAD, KULGAON, BADLAPUR (WEST) DIST-THANE 421503 EMAIL : info@reliableengineering.in.net reliableeng7@gmail.com +91-9987193247 +91-9172214249 Website:- www.reliableengineering.in.net

REPORT NO. 121 DATED 07 December 2022



<u>GEOTECHNICAL INVESTIGATION FOR</u> <u>PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED)</u> <u>AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA</u> <u>FORMASTER AND ASSOCIATES</u>

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<u>GEOTECHNICAL INVESTIGATION FOR</u> <u>PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED)</u> <u>AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA</u> <u>FORMASTER AND ASSOCIATES</u>

1.0 INTRODUCTION

Master and Associates plans to construct a material testing lab at Worli, Mumbai, Maharashtra. The proposed building will consist of double basement + Ground +7 upper floors. The work of geotechnical investigation was awarded to Reliable Engineering. The field work for the geotechnical investigation was completed by Reliable Engineeringin December 2022. This report presents results of the geotechnical investigation, along with foundation engineering recommendations for the proposed building.

2.0 EXPLORATION PROGRAM

2.1 Exploration Scope

Threeboreholes (BH-1 to BH-3) were completed for the project as illustrated on the Borehole Location Plan in the Annexure.



2.2 Subsurface Conditions

Subsurface profile at this site generally consists of fill overlying residual soil underlain bybasalt bedrock. Encountered soil/rock layers are described below;

LAYER I: FILL

Fill, consisting mostly of clay with boulders were encountered at ground surface in the boreholes. The lower boundary of this layer was encountered at a depth of 1.5m below existing ground surface.

LAYER II: RESIDUAL SOIL

Residual soils, consisting mostly of brownish stiff clay were encountered at existing ground surface in the boreholes. Based on Standard Penetration Tests (SPT) conducted within this layer, the consistency of cohesive soils was medium stiff to stiff. The lower boundary of this layer was encountered at depths of 6.2m to 6.45m below the existing ground surface.

LAYER III: BRECCIA BEDROCK

Brownish breccia bedrock was encountered at depths of 6.2m to 6.45m below existing ground surface in the boreholes. The bedrock was completely weathered to sound, generally improving with depth. Core Recoveries in the bedrock layer varied between 25% and 43%, and Rock Quality Designations (RQDs) varied between 0% and 13%. Uni-axial



compressive strength of rock core sample varied from 95kg/cm² to 106kg/cm². The boreholes were terminated in this layer at depths of 10.0m to 13.0mbelow existing ground surface.

2.3 Ground Water Table

Ground water accumulation in the borehole was monitored during and following completion of drilling activities. Groundwater was observed in boreholesat depths of 3.0m and 5.5m below ground. Seasonal and annual fluctuations in ground water levels can be expected.



3.0 FOUNDATION RECOMMENDATIONS

Completely weathered bedrock was encountered atdepths of 6.21m to 6.45mbelow existing ground surface in the boreholes. Spread/raft foundations for proposed building with double basement (at a depth of 8.0m below existing ground surface) supported on this weathered bedrock can be designed for a maximum gross allowable bearing capacity of 40 t/m².

Maximum settlement of foundations will be less than 12mm. A Modulus of subgrade reaction of 3333 t/m³ can be utilized for design of foundations.

Uniformity in the sub-stratum can be delineated upon completion of foundation excavations. It is recommended to verify the subsurface soil stratum by an experienced practicing geotechnical engineer before the completion of footings/foundations.



3.1 Basement Construction

Excavation sides should be sloped at a maximum slope of 1:1 (horizontal:vertical) or flatter within top 6.5m and 1:2 (horizontal:vertical) below this depth. If adequate space is not available for this side sloping, then excavation side shoring with bored piles should be provided.

Basement floors and walls should be adequately water-proofed. Adequate uplift resistance in the form of dead weight should be provided. Maximum groundwater table for uplift design should be taken at 1.0m below ground surface.



3.2Lateral Earth Pressures

Basement walls and pile shoring walls, if any, will be subjected to lateral earth pressures. A soil submerged unit weight (r_{sub}) and coefficient of active lateral earth pressure (k_a) of 0.8 t/m³ and 0.5, respectively, should be utilized for design of basement walls installed without adjacent pile shoring walls. Lateral earth pressure parameters for design of pile shoring walls are given in Table A below. Hydrostatic pressures and surcharge pressures, if any, should also be considered.

TABLE A LATERAL EARTH PRESSURE PARAMETERS FOR DESIGN OF PILE SHORING WALLS

Depth	Soil Type	Unit weight	Active earth pressure coefficient	Passive earth pressure coefficient	Cohesion
0.0m- 1.5m	FILL	1.8	0.4	2.5	0 t/m ²
1.5m to 6.45m	Residual Soil	1.8	0.3	3.0	0 t/m ²
Below 6.45m	Breccia bedrock	2.1	1	1	66t/m ²



3.3 Foundation Protection

Results of chemical analysis on soil and groundwater samples enclosed in the Annexure, indicate that the site falls under Class 1 for sulphate concentrations and chloride concentrations (As per IS456 and as per CIRIA Sp. Publication No. 31). A 'severe' Exposure Condition was assigned to this site. Therefore only following normal precautions are recommended to protect subsurface concrete and reinforcement.

Type of Cement:	OPC or PPC
Minimum Grade of Reinforced Concrete:	M30
Minimum Cement Content for spread foundation:	320 kg/m ³
Maximum Water Cement Ratio:	0.45
Minimum Cover to Reinforcement:	50mm



4.0 FIELD EXPLORATION PROCEDURES

The sub-surface investigation was completed generally as per IS: 1892-1979. The field investigation was carried out using rotary rigs (Calyx, 8 HP, Engine). Casing was used to support sides of borehole until sufficiently stiff strata was encountered. Standard Penetration Tests (i.e. SPT) were carried out at every 1.5m vertical interval up to bedrock, in accordance with IS 2131-1981. Using this procedure, a 5 cm outside diameter split-barrel sampler is driven into the soil by 63.5 kg. weight falling through 75 cm height. After an initial set of 15cm, the number of blows required to drive the sampler an additional 30 cm, is known as the "penetration resistance" or "N value".

After SPT refusal was obtained, NX sized rock coring was done in maximum of 1.5m runs, using diamond bit and double tube core barrel. Percent Rock Core Recovery and percent Rock Quality Designation (%RQD) were determined. % RQD = $100 \times 100 \times 10$

Sincerely,

Reliable Engineering.

TOER P.B

Mrs. Rupa Jagadale B.E (Civil) M.Tech (Geotechnical)



REFERENCES

- 1) IS 456: 2000, Plain & Reinforced Concrete Code of Practice, Fourth Revision
- 2) IS 12070: 1987, Code of Practice for Design and Construction of Shallow Foundations on Rocks
- 3) Foundation Analysis and Design, J.E. Bowles, McGraw Hill Publication, 5th Edition, 1996.



SAMPLE CALCULATION OF ALLOWABLE BEARING CAPACITY FOR FOUNDATIONS ON COMPLETELY WEATHERED BEDROCK

GL +0.0m

Layer I, Fill

-1.5m

Layer II, Residual Soil

_____-6.21m to -6.45m Layer III, Completely Weathered Breccia Bedrock

(Assuming Completely weathered Bedrock to be a very dense granular soil.)

Net Ultimate Bearing Capacity = $q_u = cNcs_c + q (N_q - 1)s_q + 0.5 B \gamma N\gamma s_\gamma$ (Refn. 5, Table 4-1)

Where,

- q = Overburden Pressure (i.e. submerged unit weight x depth of foundation)
- c = Cohesion
- B = Minimum Width of foundation = 1m
- γ' = submerged unit weight of soil = 0.80
- N_c , N_q , N_{γ} = Terzaghi's Bearing capacity factors
- Sc, sq, s_{γ} = Shape factors = Conservatively assumed as 1, 1, and 0.6
 - D = Depth of Footing Below Basement top = 1.5m

Minimum SPT N value obtained in boreholes = 50 Corresponding friction angle = 42° (Reference No. 5) Corresponding Nc=100, Nq=92, N_y=174 (Reference 5, IS:6403-1981);

Substituting these values in the above equation; q ultimate =q_u =[0x100x1]+[1.5x0.8x(92-1)x1]+[0.5x1x0.8x174x0.6]= 0+109+42 = 151 t/m² q safe = q_u/F.S. = 151/3 = 50 t/m²

Restricted to 40 t/m² to limit settlement as shown below.



CALCULATION OF SETTLEMENTS OF FOUNDATIONS (3M X 3M) EXERTING PRESSURE OF 40 T/M2:

From Reference No. 1:

Settlement =
$$S = q_0 B' \frac{1 - \epsilon^2}{E_s} m I_s I_f$$

Where,

 $\begin{array}{l} q_0 = Footing \mbox{ Pressure} = 40 \mbox{ t/m}^2 \\ B' = B/2 \mbox{ (Where B is the width of pressure distribution} \\ \mu = Poisson's \mbox{ ratio } = 0.3 \\ E = Modulus \mbox{ of Elasticity} \\ I_s = Influence \mbox{ Factor (Obtained from Table 5-2, Reference No. 1)} \\ I_f = Depth \mbox{ Factor (Obtained from Figure 5-7, Reference No. 1)} \\ m = 4 \mbox{ for center of footing} \end{array}$

Very conservatively assuming completely weathered bedrock to be overconsolidated sand:

E value for over-consolidated sand = 105(N)+4000 (Reference No. 1) Therefore, for a SPT N value of 50, E=9250 t/m²

L' = 3/2 = 1.50, B' = 3/2 = 1.5, H=6m, and D=8.0m Therefore, M=L/B=1; and N=H/B'=4, and D/B=2.67 Corresponding, I_s = 0.43, Conservative I_f = 1 (From Table 5-2, Reference 1)

Settlement of Layer =S₁= $40x1.5x \frac{1-0.3^2}{9250}x4x0.43x1 = 0.012m = 12mm$

ANNEXURE

LOCATION MAP



BOREHOLE LOGS

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 GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA

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LABORATORY TESTS



SOIL TEST DATA SHEET

IS 2720 Part 4, 5, 6

GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED)

PROJECT : AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA

CLIENT: M/s. MASTERS AND ASSOCIATES

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BH-01	1.50-2.10	SPT 1				СН	4	17	7	9	62	24	38										
BH-02	4.50-5.10	SPT 1				СН	5	19	7	6	59	22	37										
BH-03	3.00-3.60	SPT 2				СН	9	9	8	2	61	24	37										
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DS :	Direct Shear		Tcd :	Triaxial Te	st (Consolid	ated Drained)			UDS :	Undistu	irbed Sc	il Sample	e					f' :	Effective A	ngle of Interr	al Friction	
к :	Permeability Test		NP :	Non Plasti	с					VL :	Laborato	ory Vane	Shear Tes	t					Cc :	Effective Co	ohesion		
FSI :	Free Swell Test		SL :	Shrikage Li	imit Test					UC :	Unconfi	ned Com	pression T	est					>:	Combined	Silt + Clay		
								GEC) EN	GIN	EERS	S, К/	ALYA	N									

					гест	DECII	ТТС	OF DOCI		FS Agen		12 076	4 1207	20		
					1691	KL3U		OF KUC	N CUN	LO AS PE	er 15 914	13,0/0	4, 1303	50		
CLIEN	іт:	M/s. N	IASTERS AND ASS	OCIATES	5								\			
PROJ	AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA															
Sr. No.	Bore Hole No.	Core piece No.	Depth, m	Diameter, cm	Height, cm	H : D (1:H/D)	rrection Factor	ndition of Test	Failure Load	Uniaxial Compressive Strength	Point load index	Porosity	Water Absorption	Dry Density	secific Gravity	٩
				cm	cm		ပိ	රී	kN	kg/cm 2	kg/cm 2	%	%	gm/cm	SI	
1	BH-01	5	7.50-9.00	5.40	6.25	1.16	0.86	Soaked	0.8		3	4.11	1.89	2.18		
2	BH-02	6	9.00-10.50	5.41	6.10	1.13	0.85	Soaked	0.8		3	4.86	2.24	2.17		
3	BH-03	8	6.45-7.50	5.41	6.05	1.12	0.85	Soaked	0.9		3	3.80	1.72	2.21		
						C	GEO E	NGINEEF	RS, KA	LYAN						

	CHEMICAL TEST RESULT OF GROUND WATER SAMPLES.														
			As per IS 30	25 Part 11, 24, 32											
CLIENT: PROJECT:	IENT: M/s. MASTERS AND ASSOCIATES DATE 06.12.2022 ROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) DATE 06.12.2022 ROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) DATE 06.12.2022 ROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) DATE 06.12.2022 ROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) DATE 06.12.2022 ROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) DATE DATE														
SR NO.	SR NO. BH NO. DEPTH IN METERS IN METERS TYPE OF SAMPLE pH ELECTROMETERIC ALLY SULPHATE AS SO ₃ CHLORIDE AS CI ppm AS CI ppm AS CI * Limit between * Limit <400ppm														
	METERS SAMPLE * Limit between * Limit <400ppm 6.3 to 8.5 Maximum * Limit <400ppm														
1	BH-02	1.70	Water	7.01	158	289									
	1	1	GEO ENGI	NEERS, KALYAN	J										

PHOTOS

PROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA



BH-1

PROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA

BH NO. – 1

CORE BOX NO. 01 OF 01

DEPTH 0.00 TO 10.00 METER



PROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA



BH-2

PROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA

BH NO. – 2

CORE BOX NO. 01 OF 01

DEPTH 0.00 TO 13.00 METER



PROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA

BH-3



PROJECT: GEOTECHNICAL INVESTIGATION FOR PROPOSED MATERIAL TESTING LAB (2 BASEMENTS + G + 7 STORIED) AT SUDAM KALU AHIRE MARG, WORLI, MUMBAI, MAHARASHTRA

BH NO. – 3

CORE BOX NO. 01 OF 01

DEPTH 0.00 TO 10.00 METER

